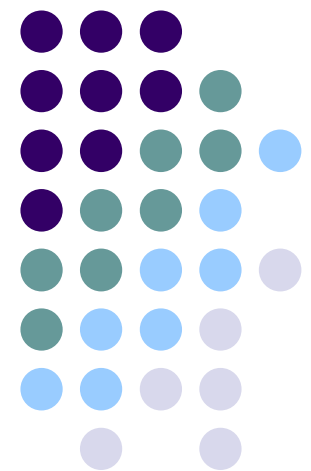
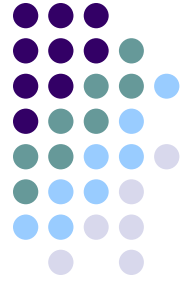


Process Control Diagram for Susceptor Assisted Microwave Heating

Shawn Allan, William Keith, Dr. Holly
Shulman
Ceralink Inc.

40th Symposium of the International Microwave Power Institute
August 11, 2006

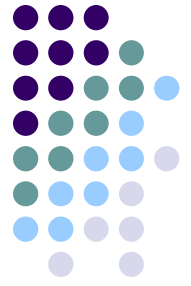




Outline

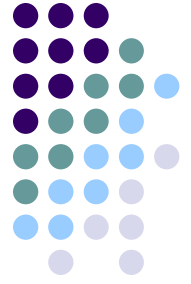
- Introduction: The need for MW susceptors for materials processing
- Variables and outputs of susceptor heating
- Relationships of volume, mass, and power to temperature, heating rate, and energy consumption
- Calculated model of temperature
- Testing of model
- Summary

High temperature microwave susceptors



- **Microwave Hybrid Heating = Susceptor + Microwave Energy**
 - Microwave : volumetric heating (coupling)
 - Susceptor: radiant heating
- **Susceptors couple well at RT**
 - Provide initial heat transfer
 - Decrease inverse temperature profile
- **Applied models will make susceptors more practical for experimental users and hobbyists**

Pros and Cons of Susceptor Heating

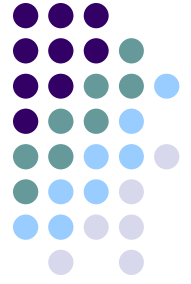


- **Pros**

- Radiant heat prevents thermal shock failures due to inverse temperature profile
- Fast, reliable way to reach high microwave temperatures quickly

- **Cons**

- Suscepting ability varies with temperature
- Susceptor heating is not always a controlled process



Model Components

- **Variables**

- Susceptor type
- Susceptor mass
- Thermal package volume
- Power input
- Time

RMS Thermcepts

m

V

P

t

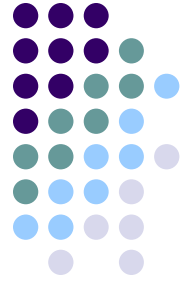
- **Outputs**

- Temperature (T)
- Heating Rate ($\partial T/\partial t$)
- Energy Consumption (E)

$$T = f(m, V, P, t)$$

$$(\partial T/\partial t) = g(m, V, P, t)$$

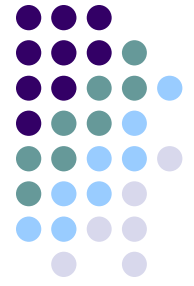
$$E = h(P, t)$$



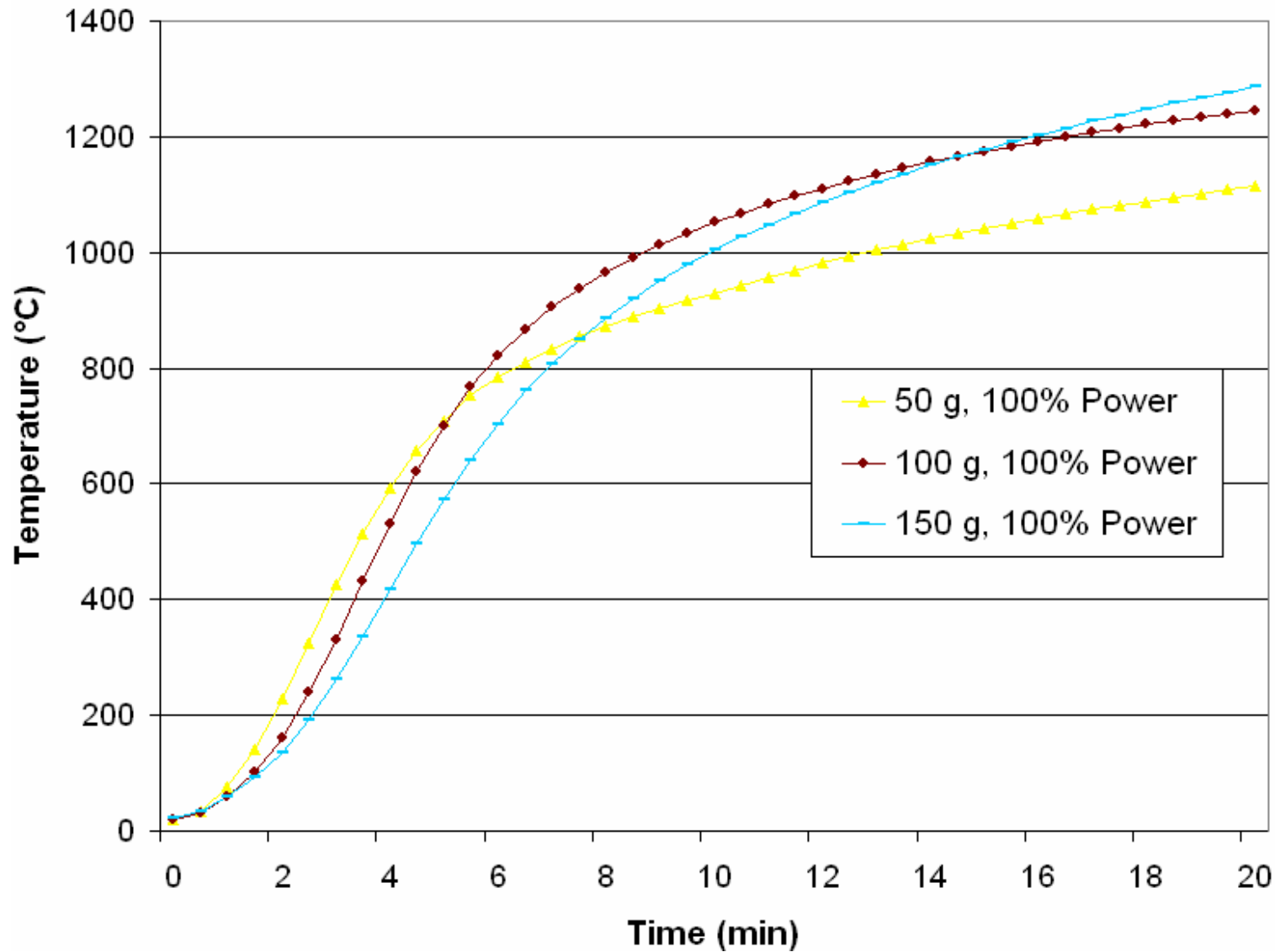
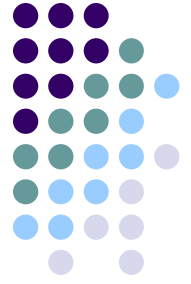
Project Goal

- Choose susceptor mass that's best for desired firing temperature!
- There is an ideal susceptor mass for different firing temperatures
 - due to inverse between susceptor mass and max heating rate for constant microwave power
 - resulting in
 - Too much susceptor slows heating initially
 - Too little susceptor slow at high temp
 - Low temp use less susceptor mass; higher temps need more susceptor mass
 - In addition
 - Maximum heating rate gives minimum energy consumption
 - Smaller volume thermal packages have higher max heating rates

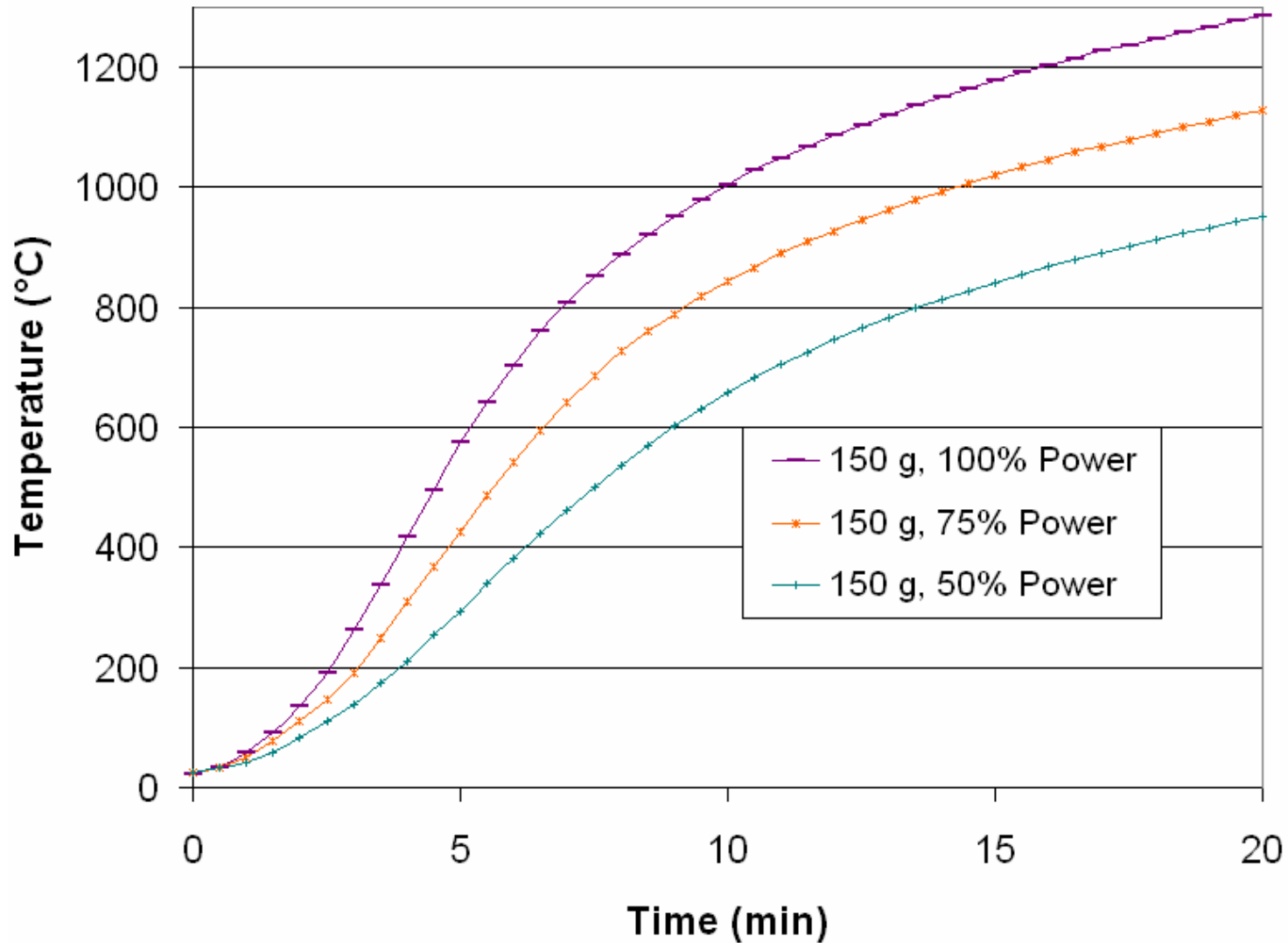
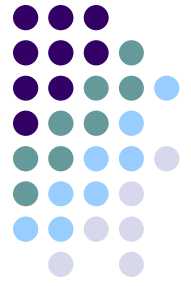
Thermwave and Susceptors



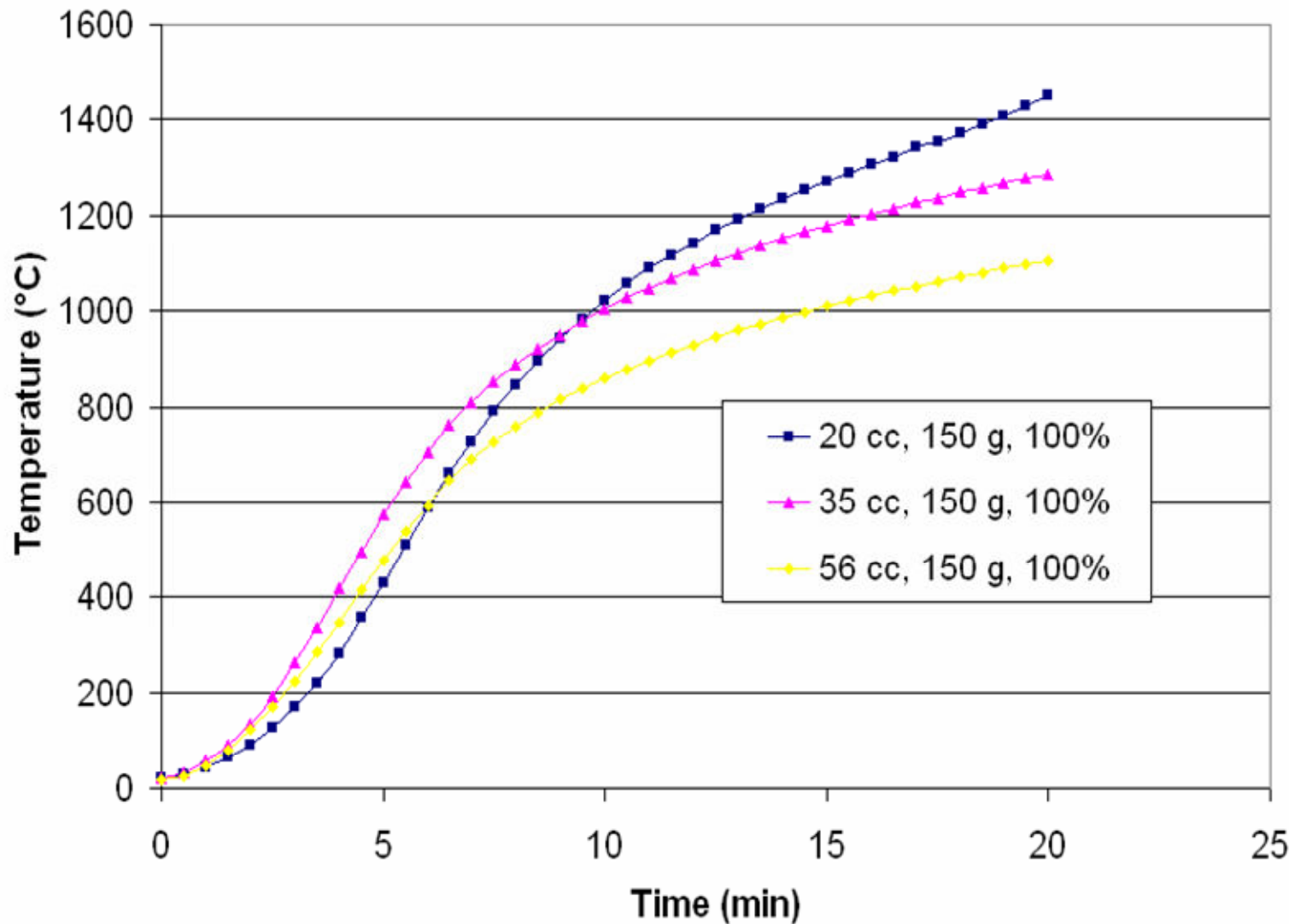
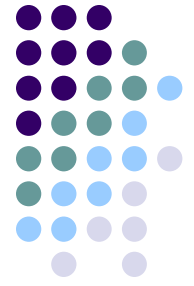
Mass Effect – Constant Power, Volume

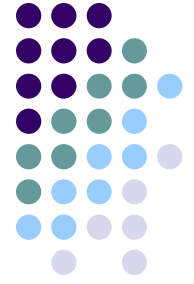


Power Effect – Constant Mass, Volume

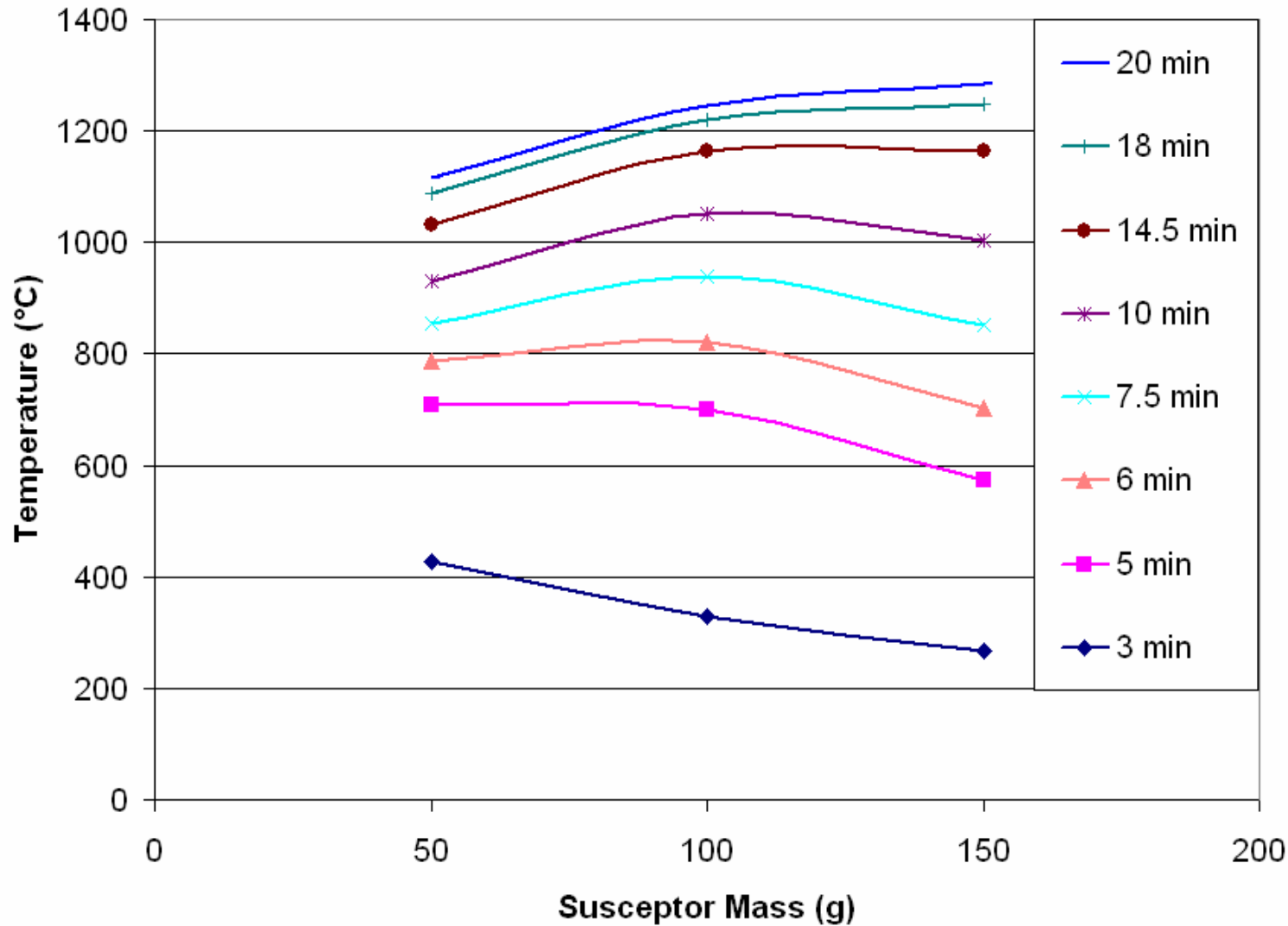


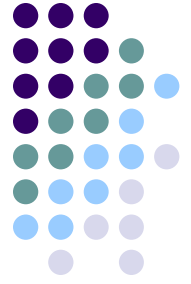
Volume Effect – Constant Mass, Power





Interaction of Mass with Time





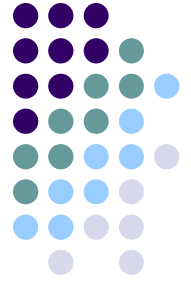
Curve Fitting $T = F(t, m, p, v)$

- Sigmoidal fitting (S-curve)

$$F(t) = c1 + \frac{(c2 - c1)}{\left(1 + \left(\frac{t}{c3}\right)^{c4}\right)}$$

- Polynomial fitting

$$T = a + bx_1 + cx_2 + dx_3 \dots nx_k$$

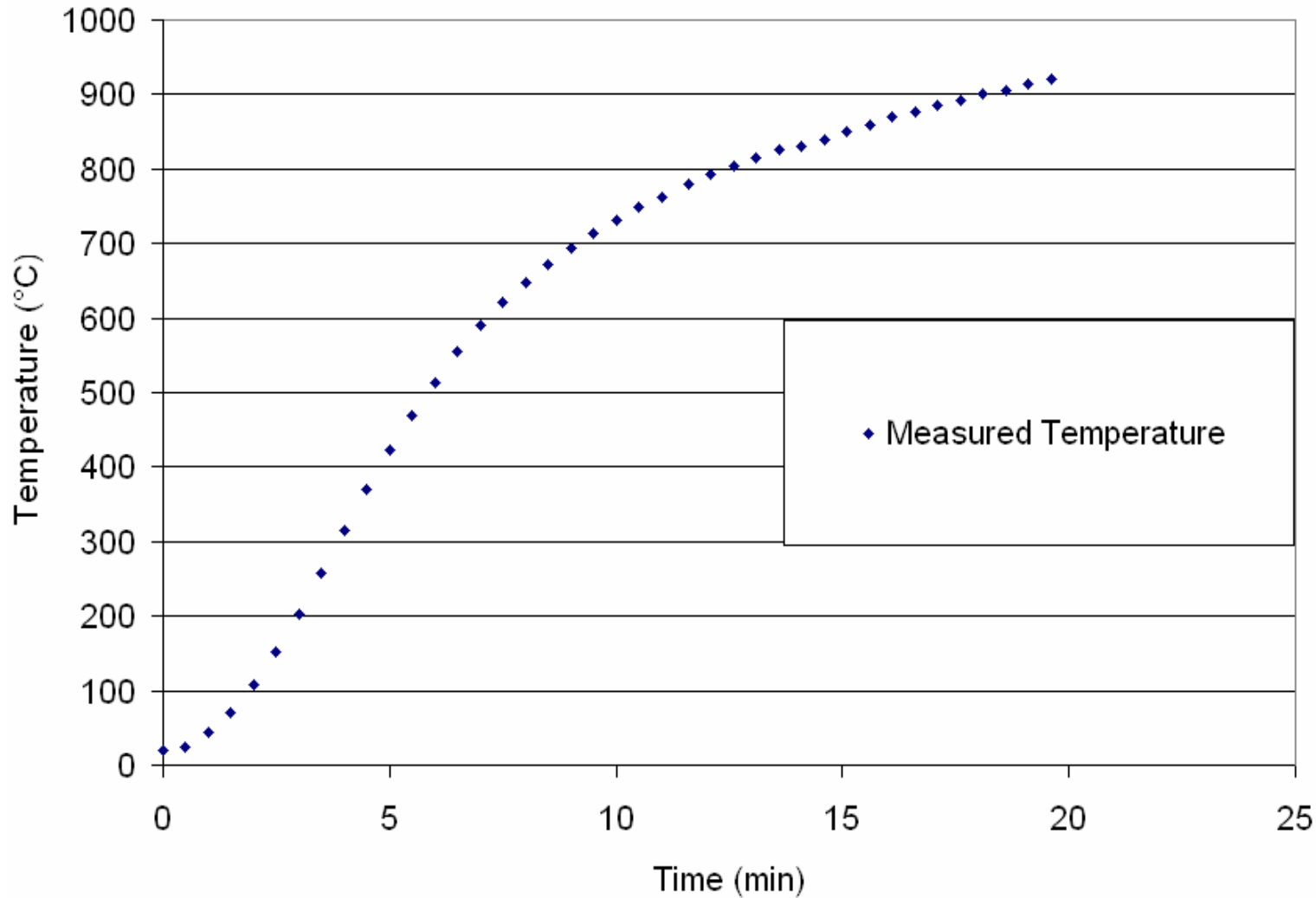
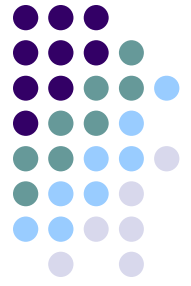


Sigmoidal Fitting

- Heating curve has sigmoidal shape
- Eventually system exhausts heating power
- When Energy In = Energy Out \rightarrow T plateau
- When $t=0$, $F(t) = c_2 = T_0 \rightarrow$ *true constant*
- Solve c_1 , c_3 , and c_4 for each T-t profile
(27 runs)
- Linear regression to determine c_1 , c_3 , and c_4
as $F(m,p,v)$, $G(m,p,v)$, $H(m,p,v)$

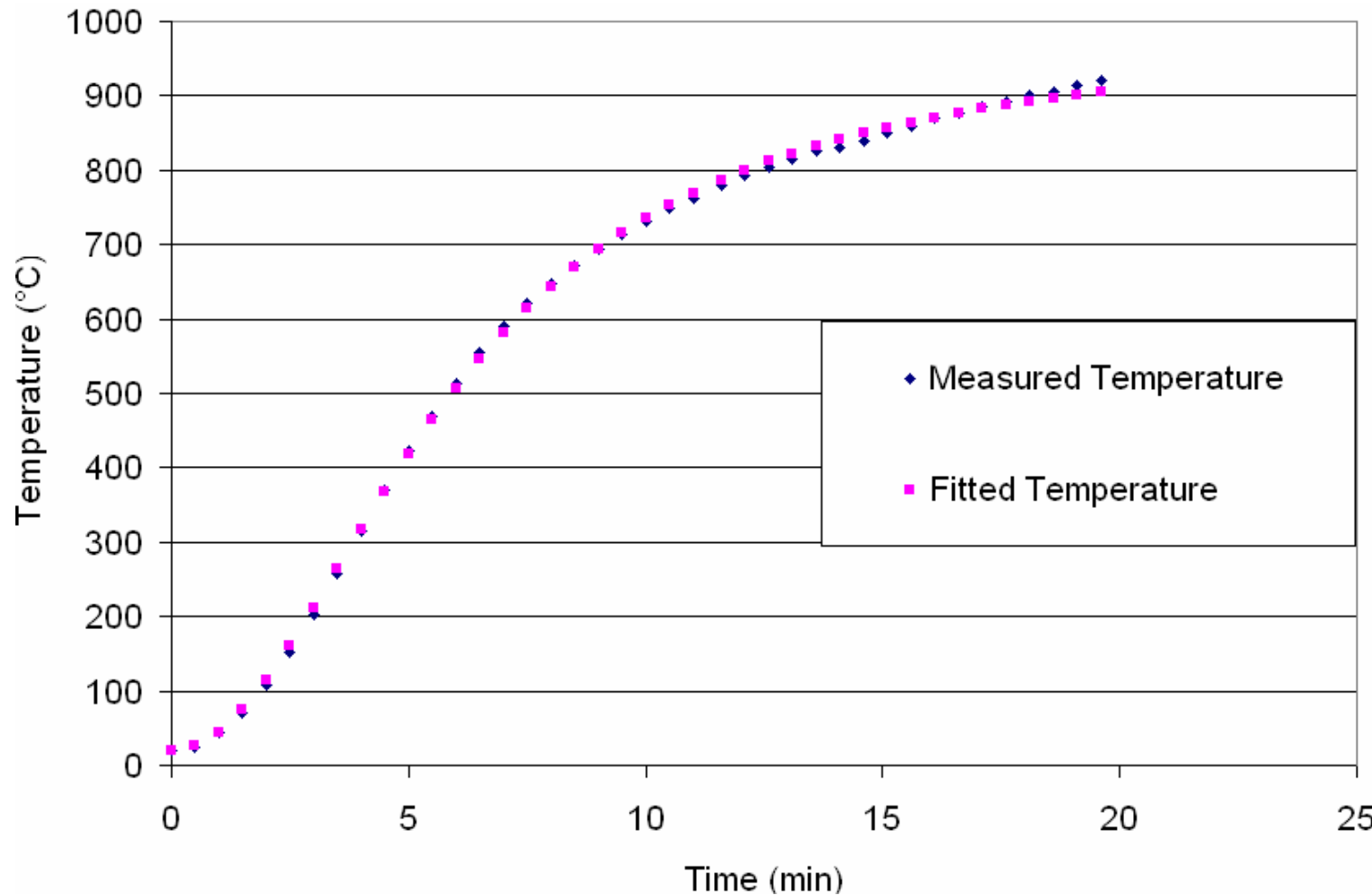
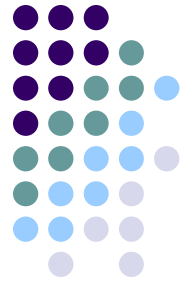
Sigmoidal Fitting

100 g, 75%, 56 cc



Sigmoidal Fitting

100 g, 75%, 56 cc



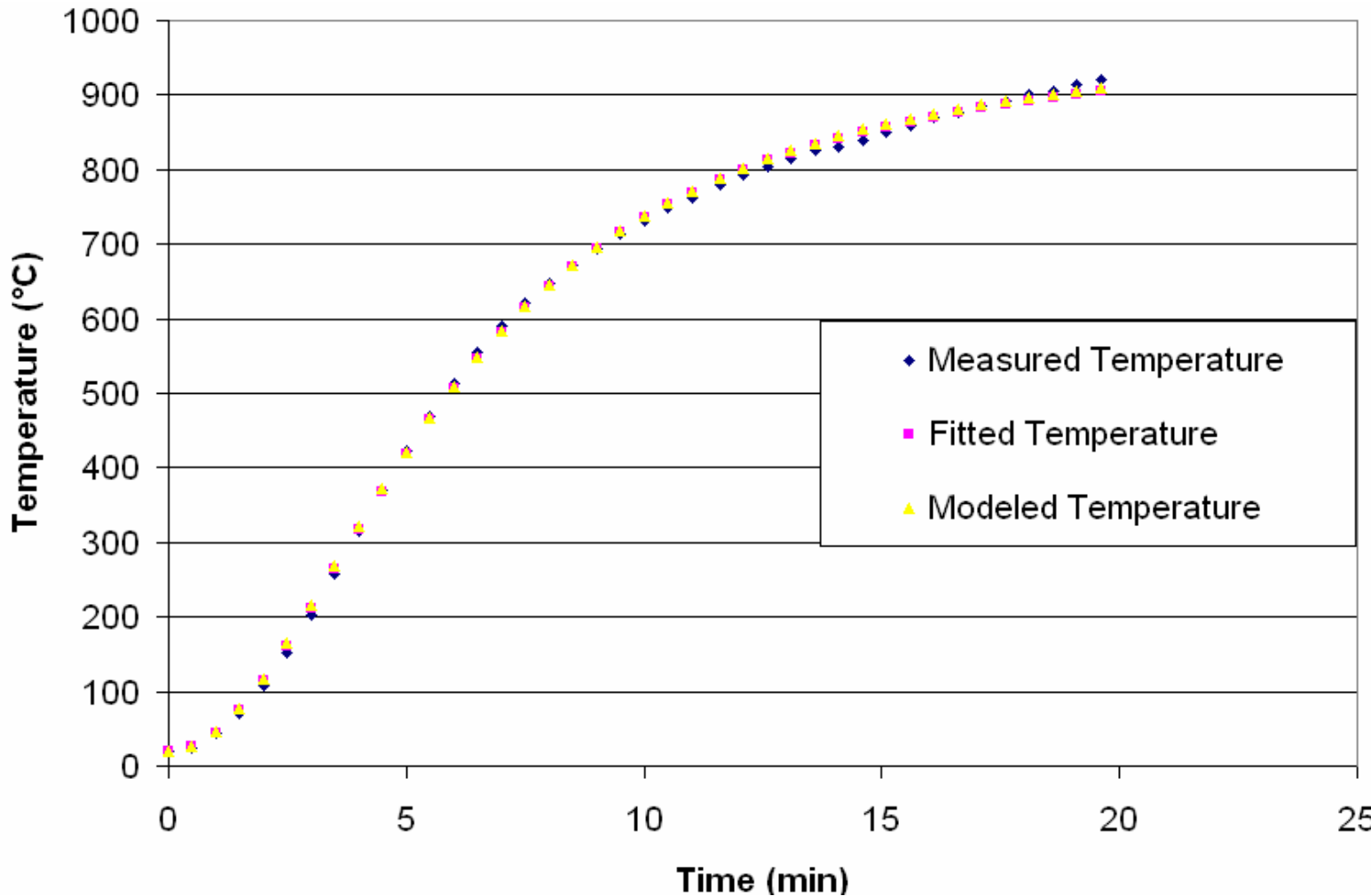
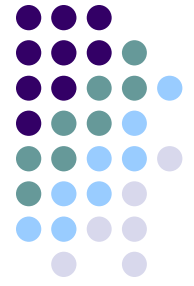
f1 = 982

f2 = 5.93

f3 = 2.04

Sigmoidal Fitting

100 g, 75%, 56 cc



f1 = 982

f2 = 5.93

f3 = 2.04



Linear regression



m1 = 991

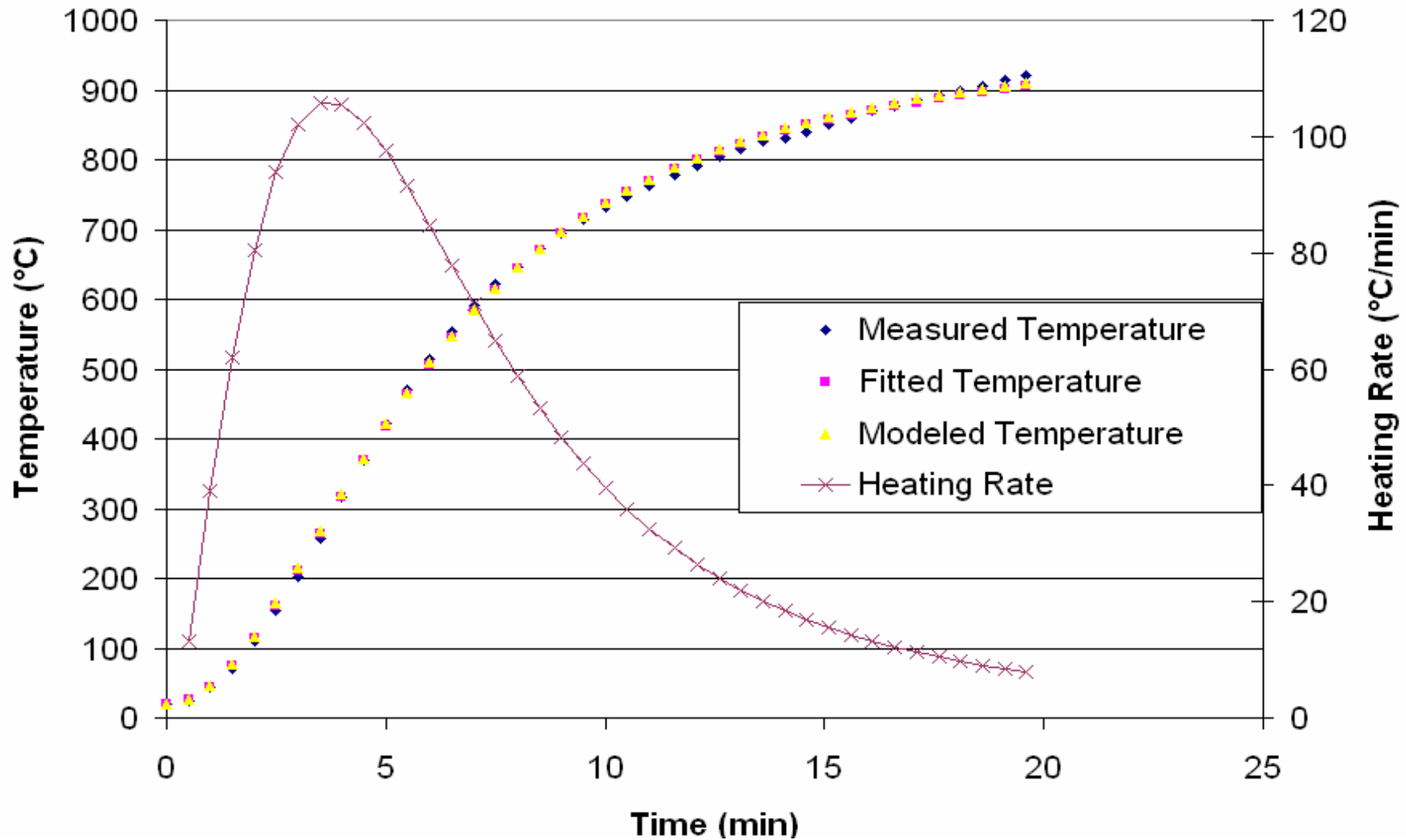
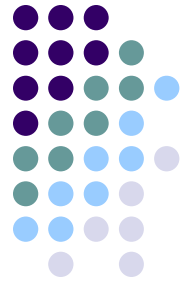
m2 = 5.96

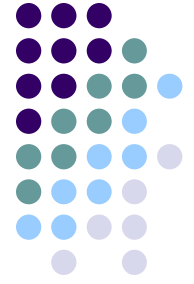
m3 = 2.01



Sigmoidal Fitting

100 g, 75%, 56 cc



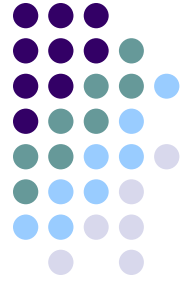


Master Fit for $T = F(t, m, p, v)$

Coded Variables	m	p	v
	-1	-1	-1
	0	0	0
	1	1	1.4

$$T = (1171 + 83.8m + 110.6p - 128.5v + 21.2mp) + \frac{(T_o - 1171 + 83.8m + 110.6p - 128.5v + 21.2mp)}{\left(1 + \left(\frac{t}{5.92 + 1.47m - 1.3p - v + 0.32pv + 0.73v^2}\right)^{2.14 - 0.091v + 0.045v^2m - 0.085m^2}\right)}$$

Master Fit for $T = F(t, m, p, v)$



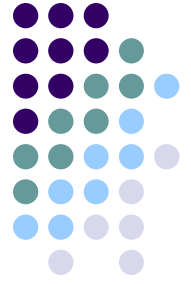
$$T = (1171 + 83.8m + 110.6p - 128.5v + 21.2mp) + \frac{(T_o - 1171 + 83.8m + 110.6p - 128.5v + 21.2mp)}{\left(1 + \left(\frac{t}{5.92 + 1.47m - 1.3p - v + 0.32pv + 0.73v^2}\right)^{2.14 - 0.091v + 0.045v^2m - 0.085m^2}\right)}$$

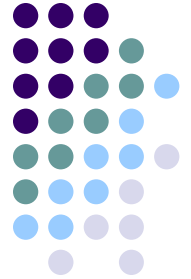
c1
c2
c1

c4

c3

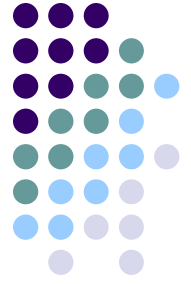
Interpolation of Master Fit





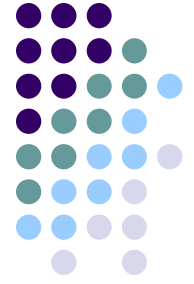
Next Steps

- **Modeling with heating load (alumina, zirconia, zinc oxide)**
- **Empirical modeling of other susceptor systems**
 - **Zirconia**
 - **Zinc oxide**
- **Transition from empirical model to physical model**
 - **Specific Heat**
 - **Activation Energy**
 - **Dielectric Properties**
 - **Conductivity**
 - **Convection**
 - **Radiation**



Conclusions

- Empirical models can be applied to high temperature susceptor assisted microwave heating
- Fit of model indicates reproducibility of susceptor assisted heating data
- Model can be used to predict heating profiles



Acknowledgements

- Dr. Timothy Keith
- John Byrnes

Questions?